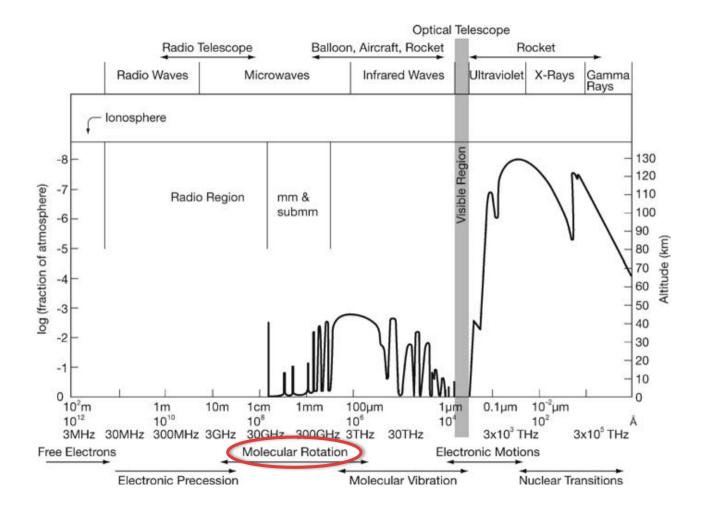
## OBSERVATIONAL METHODS IN RADIO ASTRONOMY I : SINGLE-DISH

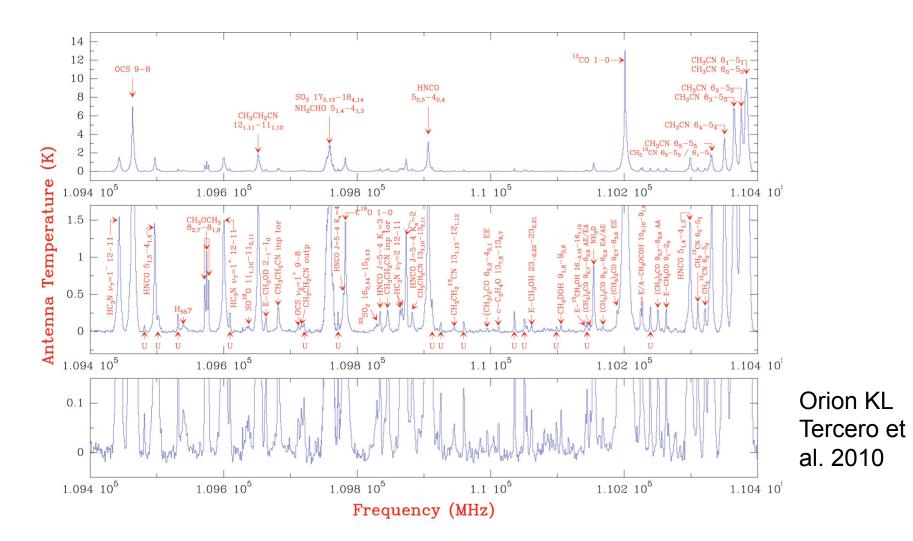


#### INTRODUCTION

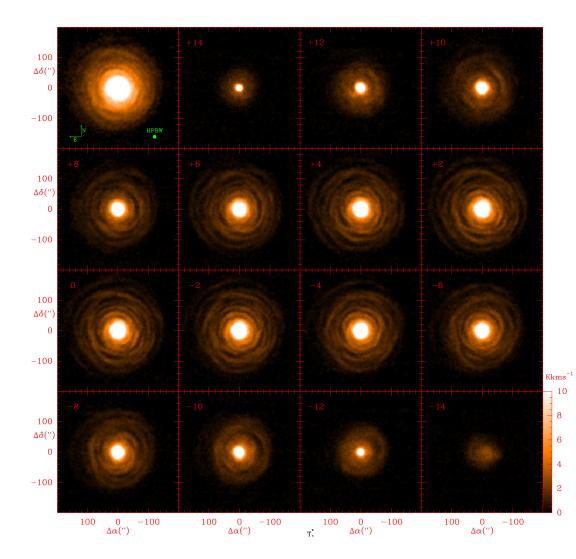
#### **THE MM-SUBMM WINDOW**



#### **THE MM-SUBMM WINDOW: spectral line surveys**



# THE MM-SUBMM WINDOW: velocity channel maps



IRC+10216; CO J=2-1 Cernicharo et al. 2015

### **GOALS / QUESTIONS**

#### Goals

- Measure the signal emitted from a particular region in the sky
- Obtain spectral or spatial information of the source
- Determine chemical and/or physical properties

Questions

- Measurement fidelity
- Calibration

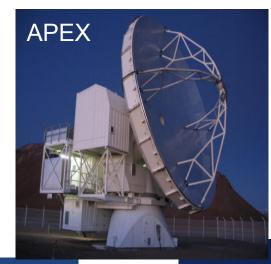
Not covered in this talk

• Receivers and backends

#### **ANTENNAS**

#### **RADIOTELESCOPES**







GBT





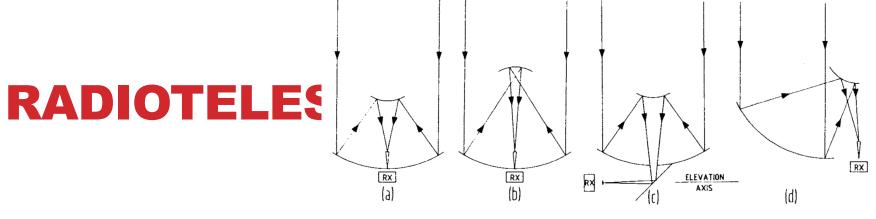


Fig. 7.6 The geometry of (a) Cassegrain, (b) Gregory, (c) Nasmyth and (d) offset Cassegrain systems

#### Parabolic primary dish, but different positions of the receivers:

- Cassegrain: hyperbolic, convex subreflector
- Gregory: elliptical, concave subreflector behind the prime focus (e.g. Effelsberg)
- Nasmyth: hyperbolic subreflector and flat tertiary mirror (e.g. IRAM 30m, APEX)
- Offset Cassegrain: "half" parabolic and hyperbolic subreflector (e.g. GBT)

#### Advantages of the different optical configurations:

- Secondary focus: 5-10 times larger f/D ratios, less sensitive to lateral focus offsets, increase effective area, decrease spillover
- Nasmyth system: receivers are not tilted with elevation, more space in rx cabin
- Offset Cassegrain: less blockage by subreflector and support structure, less standing waves

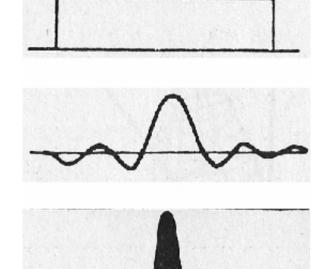
#### RADIOTELESCOPES

Obs.	D (m)	∨ <b>(GHz)</b>	λ <b>(mm)</b>	HPBW (")	Latitude (deg)
IRAM	30	70 - 345	4 - 0.7	35 - 7	+37
GTM	50 (32)	(73 – 116, 230)	4 - 0.85	20 - 6	+19
APEX	12	230 - 1200	1.3 - 0.3	30 - 6	-22
JCMT	15	210 - 710	2 - 0.2	20 - 8	+20
Herschel	3.5	500 - 2000	0.6 - 0.1	43 - 11	space
	collecting area			↓ angular resolution ~ λ/D	

#### ANTENNA THEORY: POWER PATTERN

- Reciprocity theorem: antenna in emission
- Distribution of electric field on the dish:  $E_{ant}(x, y)$
- Far field radiated by the dish:  $E_{ff}(l,m) \propto \mathcal{F}[E_{ant}(x,y)]$
- Power emitted  $\propto \left| E_{ff}(l,m) \right|^2$
- Power pattern:  $P(l,m) \propto \left| E_{ff}(l,m) \right|^2$
- Beam solid angle:  $\Omega_A = \int_{4\pi} P(\Omega) d\Omega$
- Effective area:  $A_e = \eta_A \cdot A_{geom} \rightarrow \eta_A$ : aperture efficiency

• Fundamental relation: 
$$A_e \cdot \Omega_A = \lambda^2$$



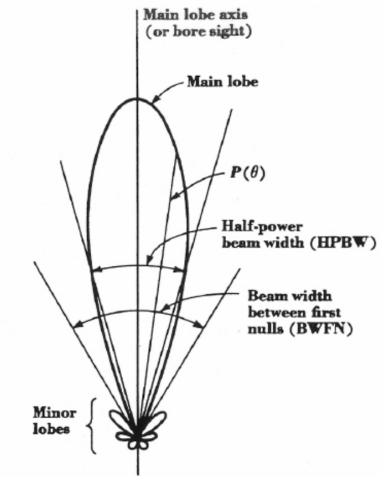
#### ANTENNA THEORY: POWER PATTERN

Main beam solid angle:

$$\Omega_{MB} = \int_{\substack{main\\lobe}} P(\Omega) d\Omega$$

Main beam efficiency:

$$\eta_B = \frac{\Omega_{MB}}{\Omega_A}$$



#### POWER COLLECTED BY AN ANTENNA

Power from a monochromatic point source, collected by an area A<sub>e</sub>:

$$p_{\nu} = \frac{1}{2} A_e \cdot S_{\nu} \quad [W \, \text{Hz}^{-1}]$$

Flux density  $S_v$  measured in Jy: 1Jy = 10<sup>-26</sup> J s<sup>-1</sup> m<sup>-2</sup> Hz<sup>-1</sup>

• If source is extended: 
$$\delta p_v = \frac{1}{2} A_e \cdot I_v \cdot \delta \Omega$$
 [W Hz<sup>-1</sup>]

Brightness  $I_{v}$  measured in Jy sr-1: 1Jy sr<sup>-1</sup> = 10<sup>-26</sup> J s<sup>-1</sup> m<sup>-2</sup> Hz<sup>-1</sup> sr<sup>-1</sup>

Source flux density is:

 $S_{v} = \int_{\Omega_{s}} I_{v}(\Omega) d\Omega$ 

BUT observed flux density is:

$$S_{obs} = \int_{\Omega s} P(\Omega) I_{\nu}(\Omega) d\Omega < S_{\nu}$$

#### **TEMPERATURE SCALES**

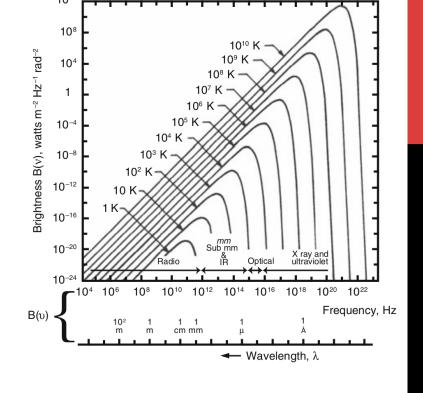
#### BLACK BODY RADIATION

Planck Law :

$$B_{\nu}(T) = \frac{2h\nu^{3}}{c^{2}} \frac{1}{e^{h\nu/kT} - 1}$$

Rayleigh-Jeans approximation:

$$hv \ll kT \rightarrow B_{\nu}(T) = \frac{2\nu^2}{c^2}kT$$



**Brightness temperature:** temperature a black body would have to match the observed intensity of an extended source at frequency v:

$$I_{\nu}(\Omega) = B_{\nu}(T_b) \quad \Rightarrow \quad T_b = \frac{c^2}{2k\nu^2} I_{\nu}(\Omega) = \frac{\lambda^2}{2k} I_{\nu}(\Omega)$$

$$S_{\nu} = \int_{\Omega s} I_{\nu}(\Omega) d\Omega = \frac{2k}{\lambda^2} T_b \Delta \Omega$$

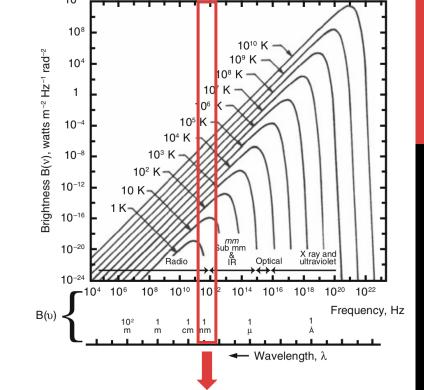
#### BLACK BODY RADIATION

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Rayleigh-Jeans approximation:

$$hv \ll kT \rightarrow B_{\nu}(T) = \frac{2\nu^2}{c^2}kT$$



Brightness temperature: temperature a bla NOTE this is not valid match the observed intensity of an extended in the mm and low T:

$$I_{\nu}(\Omega) = B_{\nu}(T_b) \quad \Rightarrow \quad T_b = \frac{c^2}{2k\nu^2} I_{\nu}(\Omega)$$

$$S_{\nu} = \int_{\Omega s} I_{\nu}(\Omega) d\Omega = \frac{2k}{\lambda^2} T_b \Delta \Omega$$

$$\frac{v}{GHz} << 20.84 \frac{T}{K}$$

At T=10K: 230 GHz~208.4K (cold dark clouds)

#### ANTENNA TEMPERATURE: T<sub>A</sub>

• Johnson noise: in thermal equilibrium, the power produced by a resistor is determined by its physical temperature:

$$p_v = kT$$
 (Nyquist theorem)

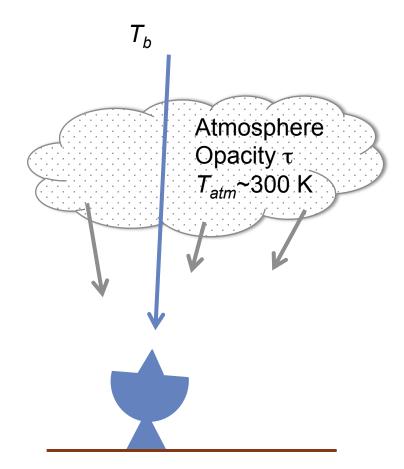
• We can define an equivalent antenna temperature:  $|p_v = kT_A|$ 

• As seen before: 
$$p_v = \frac{Ae}{2} \int_{\Omega s} P(\Omega) I_v(\Omega) d\Omega$$

$$\rightarrow T_A(\Omega) = \frac{Ae}{2k} \int_{\Omega s} I_V(\Omega) P(\Omega) d\Omega \quad \text{; using } A_e \cdot \Omega_A = \lambda^2$$

$$\rightarrow T_A(\Omega) = \frac{1}{\Omega_A} \int_{\Omega_s} \frac{\lambda^2}{2k} I_{\nu}(\Omega) P(\Omega) d\Omega = \frac{1}{\Omega_A} \int_{\Omega_s} T_b P(\Omega) d\Omega$$

### ANTENNA TEMPERATURE: *T'*<sub>A</sub>



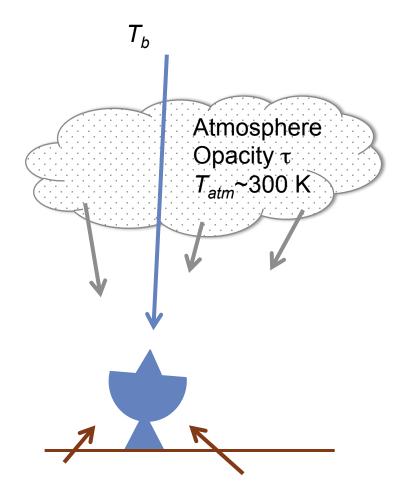
• Atmosphere effects, at a given v:

• Antenna temperature corrected by atmospheric absorption:

$$T'_A = T_A e^{-\tau_v}$$

• Note that for space telescopes, e.g. Herschel:  $T'_A = T_A$ 

### ANTENNA TEMPERATURE: *T\**<sub>A</sub>



 Correct for rear-sidelobes: measure the power received only from the forward 2π sr:

$$T_A^* = \frac{1}{P_{2\pi}} \int_{\Omega s} T_b P(\Omega) d\Omega$$

$$T_{A}^{*} = \frac{P_{4\pi}}{P_{2\pi}} T'_{A} = \frac{T'_{A}}{F_{eff}}$$

• Forward efficiency:

$$F_{eff} = \frac{P_{2\pi}}{P_{4\pi}}$$

### MAIN BEAM TEMPERATURE: T<sub>MB</sub>

- Take into account main-beam and error-lobes
- Same as  $T^*_{A}$  but within the main beam instead of  $2\pi$ :

$$T_{MB} = \frac{1}{P_{MB}} \int_{\Omega_S} T_b P(\Omega) d\Omega = \frac{P_{4\pi}}{P_{MB}} T'_A$$
  
Beam efficiency: 
$$B_{eff} = \frac{P_{MB}}{P_{4\pi}}$$

$$\Rightarrow \quad T_{MB} = \frac{T'_A}{B_{eff}} = \frac{F_{eff}}{B_{eff}} T_A^*$$

what we measure is  $T^*_A$  or  $T_{MB}$  which are NOT  $T_b$ 

- Small sources:  $\Omega_s << \Omega_{MB}$ :  $T_{MB} \approx T_b \Omega s / P_{MB} < T_b$  $\rightarrow$  beam dilution
- Large sources:  $\Omega_s >> \Omega_{MB}$ :  $T_A^* \approx T_b \int_{2\pi} P(\Omega) d\Omega / P_{2\pi} \approx T_b$
- Special case:  $\Omega_s = \Omega_{MB}$ :  $T_{MB} = T_b \int_{\Omega s} P(\Omega) d\Omega / P_{MB} = T_b$

• General case: 
$$\Omega_{s} \sim \Omega_{MB}$$
:  $T_{A}^{*} = T_{b} \int_{\Omega s} P(\Omega) d\Omega / P_{2\pi}$ 

• Usually,  $T_{MB}$  is used assuming "the source fills the beam", but...

$$\begin{array}{ccc} \Omega_{\rm s} < \Omega_{\rm MB} \rightarrow & T_b > T_{MB} \\ \Omega_{\rm MB} < \Omega_{\rm s} < 2\pi & \rightarrow & T_{MB} > T_b > T^*_A \\ 2\pi < \Omega_{\rm s} & \rightarrow & T^*_A > T_b \end{array}$$

#### **FROM KELVIN TO JANSKY**

• Flux density: 
$$S_v = \int_{\Omega s} I_v(\Omega) d\Omega = \frac{2k}{\lambda^2} \int_{\Omega s} T_b d\Omega$$

• Power received by the antenna:  $kT'_A = k \frac{T_A^*}{F_{eff}} = \frac{1}{2} A_e \cdot S_v$ 

$$\rightarrow \quad \frac{S_{\nu}}{T_A^*} = \frac{2k}{A} \frac{F_{eff}}{\eta_A} \quad \text{[Jy K-1]}$$

- Depends on the antenna
- Values are tabulated, e.g. for IRAM 30m:
   range from ~ 6 @ 90 GHz, to ~ 11 @ 340 GHz

### CALIBRATION

#### CALIBRATION

Calibration needs to account for:

- Atmosphere: Emission/absorption at frequency v ٠
  - Turbulence producing phase drifts ٠
- - Full detection system: Antenna characteristics and looses
    - Receivers: gain, noise, stability
    - Cables, backends, etc.

Questions:

- How to convert counts at the backend level, to power in ٠ physical units
- How to correct for the atmospheric contribution •

#### **CALIBRATION**

• What we measure...  $C_{sou} = \chi \Big[ T_{rec} + F_{eff} e^{-\tau_v} T_{sou} + T_{sky} \Big]$ 

where 
$$T_{sky} = F_{eff} (1 - e^{-\tau_v}) T_{atm} + (1 - F_{eff}) T_{amb}$$
  
 $T_{rec}$ : noise contribution from the receiver  
 $T_{sky}$ : noise contribution from the atmosphere  $(T_{atm})$ ,  
and the receiver cabin and ground  $(T_{amb})$   
 $\rightarrow$  Details in Lecture by Luis Velilla on friday

 Correct for atmospheric emission and stability (atmospheric and instrumental) → switching bw ON and OFF positions (observing modes)

### **CALIBRATION:** $T_{sys}$ and noise

<u>System temperature</u>: gives a measure of the noise including all sources, from the sky to backends

→ Statistical noise in our spectra (radiometer formula):

$$\sigma = \sqrt{\sigma_{on}^2 + \sigma_{off}^2} = \frac{T_{sys}}{\sqrt{d\nu \cdot \Delta t}} \text{ ; with } \Delta t = \frac{t_{on} \cdot t_{off}}{t_{on} + t_{off}}$$

$$\sigma = \frac{T_{sys}}{\sqrt{d\nu \cdot t}}$$

- dv: spectral resolution
- $t_{on}/t_{off}$ : ON/OFF integration time
- $\Delta t$ : depends on the observing mode

#### **OBSERVING MODES:** position switching

 The telescope cyclically moves between two positions, ON (Source+Atmosphere) and OFF (Atmosphere)

 $\rightarrow$  Subtracting both positions gives the source signal

- Cons:
  - OFF position without any signal → need to go far away sometimes (and spend time moving the antenna)
  - If OFF position is far, atmosphere varies  $\rightarrow$  bad baselines

• 
$$t_{on} = t_{off} = t_{tot}/2 \rightarrow \Delta t = t_{tot}/4 \rightarrow$$

$$\sigma_{psw} = \frac{2 \cdot T_{sys}}{\sqrt{dv \cdot t_{tot}}}$$

#### **OBSERVING MODES:** wobbler switching

- The secondary cyclically and quickly moves between the ON and OFF (usually symmetric OFF – ON – ON – OFF)
- Pros: very good baselines
- Cons:
  - Limited wobbling throw
  - Always in one antenna direction  $\rightarrow$  rotates in the sky
  - → Source must be compact

• 
$$t_{on} = t_{off} = t_{tot}/2 \rightarrow \Delta t = t_{tot}/4 \rightarrow$$

$$\sigma_{wsw} = \frac{2 \cdot T_{sys}}{\sqrt{dv \cdot t_{tot}}}$$

### **OBSERVING MODES:** frequency switching

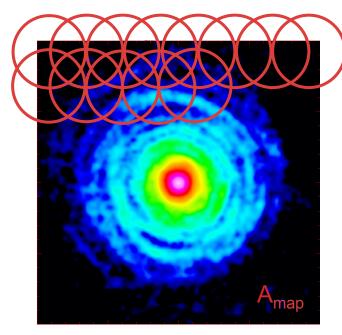
- The tuning frequency cyclically and quickly changes between two phases:  $f_{rest} f_{throw}$  and  $f_{rest} + f_{throw}$
- Pros: The telescope is <u>always</u> ON source
  - No need for OFF positions
  - Lower loise
- Cons:
  - Limited frequency throw → narrow lines
  - Presence of negative ghosts  $\rightarrow$  low line density
  - Presence of atmospheric lines
  - Strong ripples in the baselines (standing waves)

• 
$$t_{on} = t_{off} = t_{tot} \rightarrow \Delta t = t_{tot}/2 \rightarrow$$

$$\sigma_{fsw} = \frac{\sqrt{2} \cdot T_{sys}}{\sqrt{dv \cdot t_{tot}}}$$

### **OBSERVING MODES:** on-the-fly mapping

• The telescope continuously slew through the source with time to map it. The result is a cube of spectra





- Nr of independent measurements:  $n_{beam} = A_{map} / A_{beam}$
- $t_{on}^{beam}, t_{off}^{beam}: \Delta t = \frac{t_{on}^{beam} \cdot t_{off}^{beam}}{t_{on}^{beam} + t_{off}^{beam}}$
- Linear scanning speed and area speed:  $v_{area} = v_{linear} \Delta \theta$
- Nyquist sampling:  $\Delta \theta = \theta/2$

#### **OBSERVING MODES:** on-the-fly mapping

- The telescope continuously slew through the source with time to map it. The result is a cube of spectra
- Frequency switching:

$$t_{on}^{beam} = t_{off}^{beam} = t_{tot} / n_{beam} \rightarrow \Delta t = t_{tot} / 2n_{beam} \rightarrow$$

$$\sigma_{fsw} = \frac{\sqrt{2n_{beam}} \cdot T_{sys}}{\sqrt{d\nu \cdot t_{tot}}}$$

• Position switching: share same OFF for multiple ONs ON-ON-ON-OFF-ON-ON-OFF-...  $\sigma_{psw} = \frac{\left(\sqrt{n_{beam}} + \sqrt{n_{submap}}\right) \cdot T_{sys}}{\sqrt{dnut}}$ 

$$\rightarrow \frac{\sigma_{psw}}{\sigma_{fsw}} = \frac{1}{\sqrt{2}} \left( 1 + \sqrt{\frac{n_{submap}}{n_{beam}}} \right) \ge 1$$

#### **GOALS / QUESTIONS**

#### Goals

- Measure the signal emitted from a particular region in the sky
- Obtain spectral or spatial information of the source
- Determine chemical and/or physical properties

Questions

- Measurement fidelity :  $\eta_A$ ,  $\eta_B$ ,  $F_{eff}$ ,  $B_{eff}$
- Calibration
  - Gain calibration:  $C_{sou} \rightarrow T^*_A$ ,  $T_{MB} \rightarrow Sv$
  - Observing switching modes: remove noise contribution from the atmosphere and whole detection system

#### **BUT THERE'S MORE...**

- Real antenna:
  - Real beam pattern
  - Error beams
  - Antenna deformations: astigmatism, coma, etc.
- Other calibration measurements needed during observations:
  - Pointing: optimize with direction Az, El (gravity)
  - Focus: optimize secondary position in *z* (temperature)
- Receivers: e.g. *image band rejection* (SSB, DSB,..)
- Backends: bandwidth and spectral resolution

#### **FURTHER READING**

- "Tools of Radio Astronomy", T.L. Wilson, K. Rohlfs, S. Hüttemesiter A&A Library, Springer 5th Ed. 2009
- IRAM 30m and interferometry schools: <u>http://www.iram-institute.org/EN/content-page-67-7-67-0-0-0.html</u>
- NRAO Radio Astronomy essentials web course: <u>https://science.nrao.edu/opportunities/courses/era</u>
- IRAM technical reports

http://www.iram-institute.org/EN/content-page-161-7-66-161-0-0.html