Miniaturized Metamaterial Filters Using Ring Resonators

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Abstract — In this paper extremely compact metamaterial closed loop resonators are demonstrated and implemented in a 3 pole Chebyshev filter and a 4 pole quasi elliptic filter at 800MHz for mobile communications. Simulated and experimental results are shown.

I. INTRODUCTION

Metamaterials (MTM) were envisioned by Veselago's investigations in which materials displaying negative permittivity (ε) and permeability (μ) simultaneously were reported giving rise to waves with antiparallel group velocity (v_{σ}) and phase velocity (v_n) , and hence having a negative refractive index [1]. Experimental demonstrations of such properties were not achieved until 30 years later when an effectively homogenous structure, able to propagate MTM waves was proposed [2]. In 2002, a new engineering approach to Left Handed (LH) structures was shown by arranging lumped inductors and capacitors [3]. The unique electromagnetic properties of MTM allow breakthrough improvements in microwave subsystems performance [4]. In particular, for filter applications, metamaterials offer circuit miniaturization and no harmonic generation [5]-[9]. In modern mobile phone systems such as B3G/4G, frequencies in the range of 400MHZ, 700MHz and 800MHz have been allocated [10]. Since these bands are relatively low to avoid atmospheric attenuation, filter miniaturization is essential. Moreover, to achieve ultra high speed data transfer rates, these systems will also require parallel processing of higher frequency bands (2.3-2.4GHZ and 3.4-3.6GHz [10]) for which filters with no harmonic generation will be key components to avoid interference between the lower and higher bands.

Circular ring resonators have been well studied in the literature for mono and dual band filters [11]-[18]. These consist of a 360° looped transmission line. However, one of their main drawbacks is their large size. By using MTM structures miniaturization can be achieved [9]. In a MTM ring resonator a LH MTM transmission line is cascaded with a conventional (RH) transmission line, both having the same phase-shift magnitude but with opposite signs therefore giving rise to a zeroth order resonance at the center frequency [7].

To date, no high performance filters have been reported in the literature using MTM ring resonators. In this paper a 3 pole Chebyshev and a 4 pole quasi elliptic filters are demonstrated at 800MHz achieving a 90% miniaturization compared to conventional structures. Simulation and experimental results will be exhibited showing good agreement.

II. CRLH RING RESONATOR DESING

The first step was to design a Composite Right Left Hand (CRLH) balanced transmission line using Rogers DUROID 5880, $\varepsilon_r = 2.2$, and h = 1.575 mm. The structure was designed at 50 Ω , with two cells N = 2, and a phase of 0° at the center frequency $f_0 = 860$ MHz. The phase shift of the LH is +111°. The values for the LH line are calculated following the procedure shown in [3] and are: C_L = 3.96854pF, and L_L = 9.921nH. Then this structure is cascaded with a conventional RH transmission line with a phase shift -111° and looped together as shown in Fig. 1. Each LH cell is implemented in a "T" type configuration with two series capacitors of value $2C_L$ and a shunt inductor of value L_L . The lumped elements were realized with standard Surface Mounted Devices (SMDs). This resonator is 80% smaller than a conventional ring resonator.

To measure the unloaded quality factor this resonator was weakly coupled to the input transmission lines and simulated in a metallic enclosure using [19]. Then it was implemented and measured using a Vector Network Analyser (Wiltron model 360B). Fig. 1a shows a picture of the final resonator. Fig. 1b exhibits the experimental and simulated results. The simulated center frequency is $f_0 = 886$ MHz, whereas the experimental is $f_0 = 820$ MHz. Since the length of the SMDs is not considered in the simulator this frequency shift is expected. Moreover manufacturing and material tolerances exist. The simulated unloaded Q_0 is 65.09. And the experimental is $Q_0 = 40$.

At around 2.8GHz the length of the looped resonator is equivalent to 360° in terms of electrical length, hence generating the first spurious resonance as shown in Fig. 1c.

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Fig 1. (a) CRLH Ring Resonator Layout. (b) Measured and simulated insertion loss of CRLH ring resonator in narrow band with measured $Q_{un} = 39.04$ and Simulated $Q_{un} = 65.6$. (c) Measured and simulated insertion loss of CRLH ring resonator in wide band with $f_b > 3f_R$.

(c)

Frequency (GHz)

III. 3 POLE CHEBYSHEV FILTER

The values of a low pass prototype Chebyshev filter of third order for a 0.1dB ripple are $g_0 = g_4 = 1$, $g_1 = g_3 = 1.0316$ and $g_2 = 1.147$ [20]. And by using equations 1 and 2 for a fractional bandwidth FBW of 7%, and $f_0 = 859$ MHz the parameters of the filter can be extracted.

$$k_{i,j+1} = \frac{FBW}{\sqrt{g_i g_{i+1}}}$$
, from $i = 1$ to *n*-1. (1)

$$Q_{e1} = \frac{g_0 g_1}{FBW} \tag{2}$$

where Q_{el} and Q_{en} are the external quality factors, $k_{i,j+1}$ are the coupling coefficients between resonators. The final values are as follows $Q_{el} = Q_{e3} = 14.7371$ and $k_{l,2} = k_{2,3} = 0.064340$.

To determine the respective coupling configurations, a full wave simulator was used. Due to the extremely small size of the resonator strong couplings are difficult to realize. To achieve the desired Q_e , the input transmission line was inserted through underneath the SMD capacitor looping the resonator as shown in Fig. 2a. For the external coupling, extra coupling transmission lines were added to achieve the required *k* coupling as exhibited in Fig. 2b.



Fig. 2. Coupling configurations. (a) To achieve the desired Q_{e} . (b) To achieve the required k coupling.

The final filter layout is shown in Fig. 3a and the simulated and experimental results in Fig. 3b. It is seen that the simulation including losses had a BW of 84MHz (896-811MHz) with an insertion loss of -2.98 dB at the center frequency and a return loss greater than -14.35 dB throughout the band. While the experimental results had a BW of 99MHz (824-725MHz, 12.7%) with an insertion

loss of -2.2 dB at the center frequency and a return loss greater than -15 dB. It is believed that the simulated insertion losses are higher since the actual SMD Q factors are higher than the specified by the manufacturer. There was a frequency shift of 84MHz due to the SMD components.





Fig. 3. (a) Final 3 Pole Chebyshev Filter layout. (b) Simulated and experimental results.

IV. 4 POLE QUASI ELLIPTIC FILTER

The low pass prototype elements for a 4th order quasi elliptic filter with a ripple of 0.044dB are [21], $\Omega_a = 1.8$, $g_1 = 0.95974$, $g_2 = 1.42192$, $J_1 = -0.21083$, $J_2 = 1.11769$. In the same way as in the 3 pole filter, the parameters are calculated for a FBW = 7.2% at a center frequency $f_0 =$ 859MHz. The final values are: $Q_{e1} = Q_{e4} = 13.3297$, $M_{l,2} = M_{3,4} = 0.06163$, $M_{2,3} = 0.056595$ and $M_{l,4} = -0.015816$. Similar coupling schemes as for the previous filter were used to achieve tight couplings. To accomplish a negative coupling the line between resonators 1 and 4 is made 180° longer. The final layout of the filter is shown in Fig. 4a and the experimental and simulated responses in Fig. 4b. The simulated BW was 63MHz (824 - 887MHz or 7.33%) with an insertion loss of -3.65 dB at the center frequency and a return loss greater than -22.62 dB in the pass band. For the experiment, the BW was 80MHz (740-820MHz or 10.2%) with an insertion loss of -2.6 dB and an insertion loss lower than -15 dB. There was a 76MHz frequency shift caused mainly by the SMD components.



Fig. 4. (a) Final 4 Quasi Elliptic Filter layout. (b) Simulated and experimental results.

V. CONCLUSIONS

MTM closed loop resonators have been demonstrated with a miniaturization of 80% at the 800MHz band and without harmonic generation. Using these resonators two filters (one 3 pole Chebyshev and a 4 pole quasi elliptic) were successfully implemented showing good agreement between simulation and experiment.

References

- V.G. Veselago, "The electrodynamics of substances with simultaneously negative values of ε and μ," Soviet Physics Uspekhi, vol. 10, no. 4, pp. 509–514, Jan., Feb. 1968.
- [2] R. A. Shelby, D. R. Smith, and S. Schultz, "Experimental verification of a negative index of refraction," *Science*, vol. 292, pp. 77–79, April 2001.
- [3] C. Caloz and T. Itoh, "Application of the transmission line theory of left-handed (LH) materials to the realization of a microstrip LH transmission line," in *Proc. IEEE-AP-S* USNC/URSI National Radio Science Meeting, vol. 2, San Antonio, TX, pp. 412–415, June 2002.
- [4] C. Caloz and T. Itoh, "Novel microwave devices and structures based on the transmission line approach of metamaterials," in *IEEE-MTT Int'l Symp.*, vol. 1, Philadelphia, PA, pp. 195–198, June 2003.
- [5] Christophe Caloz and Tatsuo Itoh. *Electromagnetic Metamaterials: Transmission Line Theory and Microwave Applications*, December 2005, John Wiley & Sons, Inc.
- [6] Samer Abielmona, Hoang V. Nguyen, Christophe Caloz, "CRLH Zeroth Order Resonator (ZOR): Experimental Demonstration of Insensitivity to Losses and to Size," *Proceedings of Asia-Pacific Microwave Conference 2006*, APMC 2006. Yokohama, Japan, pp. 657-662. 12-15 Dec. 2006
- [7] A. Sanada, C.Caloz and T. Itoh, "Zeroth order resonance in composite right left handed transmission line resonators," *Proc. Asia-Pacific Microwave Conference*, Seoul Korea, 2003. vol. 3 pp 1588-1592.
- [8] Hui Feng Ma, Xian Qi Lin, Di Bao, Tie Jn Cui, "Zeroth-Order Resonators Using Novel Compact Meta-Structures," *International Symposium on Biophotonics, Nanophotonics* and Metamaterials 2006. Hangzhou, China. 16-18 Oct. 2006. pp. 533-535
- [9] Catherine A. Allen, Kevin M. K. H. Leong, Tatsuo Itoh, "Design of Ring Resonator Mode Spacing and Bandwidth using the Phase Response of Composite Right/Left Handed Transmission Lines," *IEEE MTT International Microwave* Symposium, 2005.
- [10] Ferdo Ivanek, "Convergence and competition on the way toward 4G," *IEEE Microwave Magazine*, vol 9, Issue 4, August 2008, pp. 6-14.

- [11] L. Hsieh and K. Chang, "Dual-mode quasi-elliptic- function bandpass filters using ring resonators with enhancedcoupling tuning stubs," *IEEE Trans Microwave Theory Tech*, vol. 50, Issue 5, May 2002, pp. 1340–1345.
- [12] J.S. Hong and M.J. Lancaster, "Realization of quasi-elliptic function filter using dual-mode microstrip square loop resonators," *Electronics Letters*, vol. 31, Issue 24, 23 Nov 1995, pp. 2085–2086.
- [13] A. Abramowicz, "Investigation of the HTS microstrip filters based on dual-mode ring resonators," 12th Int Conf Microwaves and Radar MIKON '98, 1998, pp. 8–12.
- [14] L. Hsieh and K. Chang, "Compact dual mode elliptic function bandpass filter using a single ring resonator with one coupling," *Electronics Letters*, vol. 36, Issue 19, 14 Sep 2000, pp. 1626–1627.
- [15] A. Goʻruʻr, "Description of coupling between degenerate modes of a dual mode microstrip loop resonator using a novel perturbation arrangement and its dual mode bandpass filter applications," *IEEE Trans Microwave Theory Tech*, vol. 52, Issue 2, Feb 2004, pp. 671–677.
- [16] Hennings, "Design optimization of microstrip square ring bandpass filter with quasi elliptic function," *33rd European Microwave Conference*, Munich, vol. 1, 7-9 Oct. 2003, pp 175–178.
- [17] A Corona-Chávez, et.al., "Novel Dual-mode ring resonators with very low sensitivity to substrate thickness," *Microwave and Optical Technology Letters*, Wiley-Interscience, November 2005, pp. 381-384.
- [18] Corona-Chavez, M.J. Lancaster and H.T Su, "HTS Quasi-Elliptic filter using capacitive-loaded cross-shape resonators with low sensitivity to substrate thickness," *IEEE Trans. on Microwave Transactions and Techniques*, January 2007, vol. 55, pp. 117-120.
- [19] Sonnet 7.0b, EM suite, Sonnet Software Inc.
- [20] G. L. Matthaei, L. Young, and E. M. T. Jones, *Microwave Filters, Impedance-Matching Networks, and Coupling Structures*, Artech House, 1980.
- [21] Jia-Shen G. Hong and M. J. Lancaster, *Microstrip filters for RF/Microwave Applications*, John Wiley & Sons, New York, 2001.